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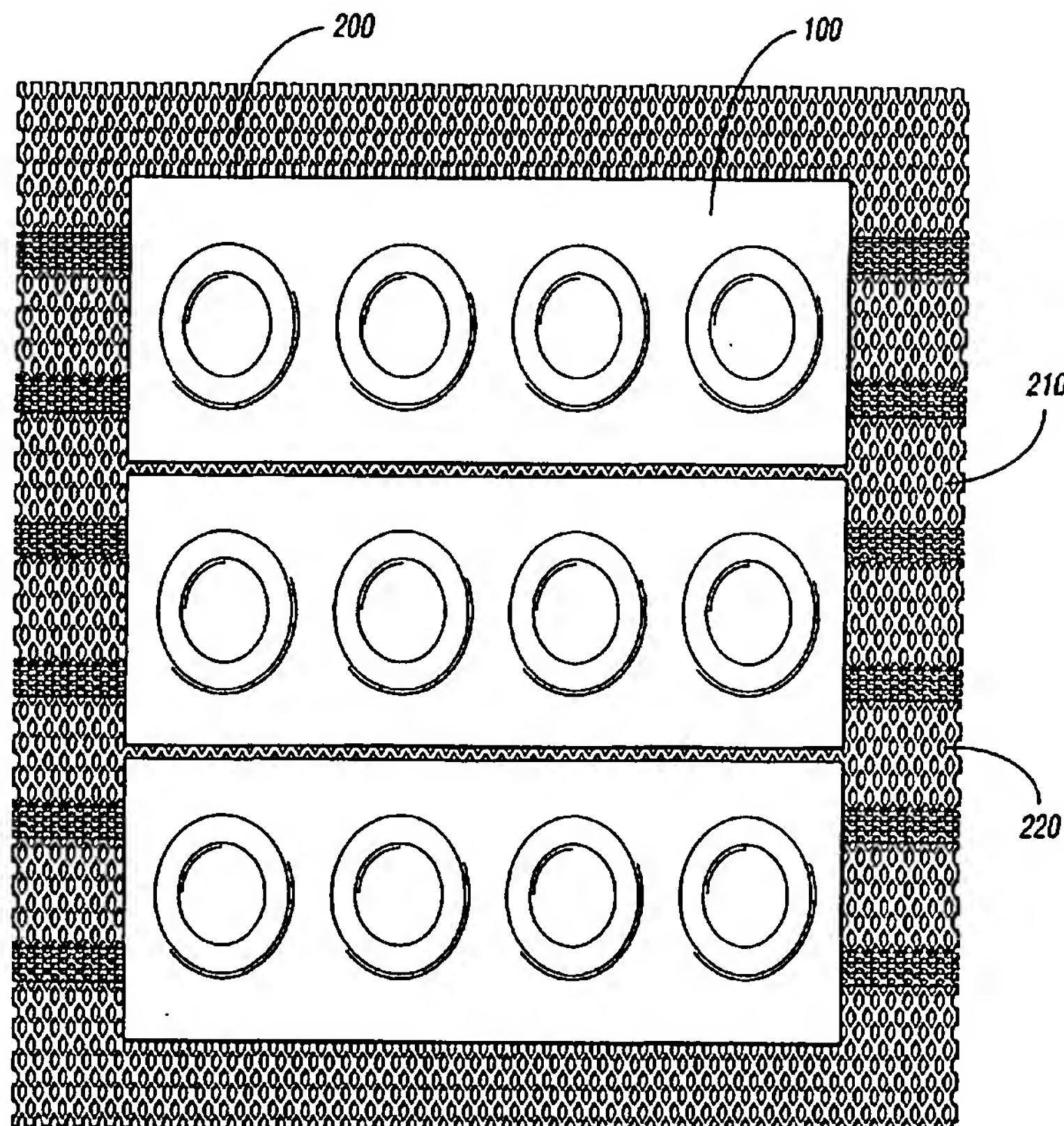
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(54) Title: COMPOSITE ENERGY ABSORBER



(57) Abstract: A composite modular energy absorbing assembly with one or more gamma structures 100 that are interposed with one or more delta structures 200. The gamma structures have a base 12' and a plurality of recesses 16' defined therewithin. The recesses 16' have at least one wall 20' extending from the associated base 12'. At least some of the recesses 16' are oriented such that their walls are substantially parallel to a major incident component of an impacting force. The walls 20' collapse. The delta structures 200 have a lattice 210 of interconnected strands which intersect to define a plurality of cells 220. The plane of at least some of these cells are substantially parallel to the impacting force. The lattice collapses during energy absorption. The composite assembly serves to decelerate an object that impacts thereupon in order to maximize energy absorption over a given distance. In alternate embodiments, stacking arrangements include: gamma structures alone; or delta structures alone.

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COMPOSITE ENERGY ABSORBER

BACKGROUND OF THE INVENTION

1. Field of the Invention

5 This invention relates to a composite energy absorber for decelerating an object that impacts the absorber.

2. Background Art

The prior art discloses numerous devices that absorb mechanical energy in various applications. Examples include protective packaging used in shipping containers, crash helmets, bumpers and vehicular interior components. Ideally, the most efficient energy absorber exerts a constant resistive force to decelerate an impacting object over the distance that the impacting object displaces the incident surface of the absorber. The most efficient curve would have a constant slope of zero. As an example, elastomeric solids many times act as springs where the force-deflection curve is essentially a straight line of a given slope. Many foam materials display a similar force-deflection curve, although the curves are usually of not of constant slope.

U.S. Patent No. 3,933,387, entitled "Thermoformed Plastic Energy Absorber For Vehicles" concerns energy absorbing media that disclose identical truncated pyramids that extend from layered sheets of plastic stock which intermesh and mutually support each other. (*Id.*, Col. 1, ll. 7-9; Col. 3, ll. 20-22.) The reference teaches that multiple sets of sheets may be stacked adjacent to each other in order to create an absorber within which the energy is absorbed. The pyramids of each sheet project onto the design quadrilateral of the opposing sheet and the edges of each pyramid contact the corresponding edges of the surrounding four pyramids. (*Id.*, Col. 3, ll. 32-36.)

Commonly owned U.S. Patent No. 5,700,545, entitled Energy Absorbing Structure, discloses an energy absorbing device that offers a nearly

constant resistance force over a deflection distance, which if exactly constant, would be theoretically most efficient in absorbing energy. The disclosure of this patent is incorporated herein by reference. Energy is absorbed by a lattice of interconnected strands of material with apertures between the strands, such that upon deformation
5 the strands at least partially coalesce and the apertures at least partially close.

Commonly owned U.S. Patent No. 6,017,084 discloses stranded structures that are oriented such that nearly all the metal structure is substantially in the crush plane. The strips of stranded metal are connected by the incident member. This reduces cost and weight of the assembly.

10 Commonly owned U.S. Patent No. 6,199,942 describes a structure wherein the stranded metals are assembled into channels in a base and/or a structure of recesses formed in the base. Either or both structures may provide impact protection.

These and other energy absorbing members, in the automobile
15 environment, are used to protect vehicle occupants and may be used in applications to meet the standard for head injury protection for automotive interiors (Federal Motor Vehicles Safety Standard 201) which is incorporated herein by reference. The standard requires that interior components must be tested using a 10 lbm headform impacting the surface at 15 mph. A measurement of HIC(d) (head injury criteria
20 (dummy)) is determined according to a formula set forth in FMVSS 201. The value of HIC(d) should not exceed 1000.

The prior art leaves unsolved production problems that stem from relatively expensive and in some cases, less effectual approaches. Injection molding, reaction molding, extruding, blow molding, honeycomb formation, and stranded
25 metal manufacture can be relatively costly. Additionally, it can be difficult to mold very thin wall thickness with some molding technologies.

In light of these and related approaches, there remains the desire to absorb as much impact energy in as little crush distance as possible, with as little

weight that is necessary, yet be capable of being manufactured under favorable economic conditions.

SUMMARY OF THE INVENTION

It is an object of the present invention to provide a more cost
5 effective, efficient energy absorber.

The invention includes a composite modular energy absorbing assembly comprising interposed structures, termed herein as "gamma" and "delta" structures. The gamma structures have a base and recesses defined within the base. The recesses include a wall extending from the base. In some cases, the wall
10 collapses partially plastically and partially elastically in order to provide some spring-back following deformation. The gamma structure is similar to the second structure depicted in commonly owned U.S. Patent Number 6,199,942.

The delta structures are positioned in operative engagement with the gamma structures. The delta structures have a lattice of interconnected strands which intersect to define cells. Some of the cells are oriented in a plane that is substantially
15 parallel to the impacting force. Like the gamma structure, cells collapse partially plastically and partially elastically during energy absorption. Energy absorption by the delta structure is maximized over a given distance.

BRIEF DESCRIPTION OF THE DRAWINGS

20 FIGURE 1 is a quartering perspective view of a modular energy absorbing assembly manufactured in accordance with the present invention;

FIGURE 2 is a bottom plan view thereof;

FIGURE 3 is a cross-sectional view of the invention depicted in Figure 2, taken along the 3-3 thereof;

FIGURE 4 is a quartering perspective view of an alternate embodiment of the disclosed invention;

FIGURE 5 is a cross-sectional view of the embodiment depicted in Figure 4 taken along the line 5-5 thereof;

5 FIGURE 6 is a quartering perspective view of a second alternate embodiment of the disclosed invention;

FIGURE 7 is a cross-sectional view taken along the line 7-7 of the embodiment of Figure 6;

10 FIGURE 8 is a quartering perspective view of a third alternate embodiment of the disclosed invention;

FIGURE 9 is a cross-sectional view taken along the 9-9 of the embodiment depicted in Figure 8;

FIGURE 10 is an end elevational view of a composite modular energy absorbing assembly which includes interposed gamma and delta structures;

15 FIGURE 11 is a top elevational view thereof;

FIGURE 12 is a bottom elevational view thereof;

20 FIGURE 13 is a partial cross-sectional view of an alternate embodiment of the invention wherein adjacent bases of two gamma structures are placed in operative engagement with each other, and the associated floors are spaced apart;

FIGURE 14 is a partial cross-sectional view of nested gamma structures wherein the floors of adjacent gamma structures are in juxtaposition and associated bases are in juxtaposition; and

FIGURE 15 is a partial cross-sectional view of a still further alternate embodiment wherein the floors of adjacent gamma structures are in juxtaposition.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring first to Figures 1-3 of the drawings, there is depicted a modular energy absorbing assembly 10 which has a base 12 and at least one energy absorbing module 14 associated with the base for accommodating deformation of the assembly. Figures 1-3 depict what is termed herein as a "gamma" structure 11 (Figures 10-12). Each energy absorbing module 14 has a plurality of recesses 16 defined within and integral with the base. At least some of the recesses have a substantially flat, or domed floor 18, and at least one wall extending from the floor to the base. Interposed between the floor 18 and the at least one wall is an intermediate segment 22. The intermediate segment has an average radius (R), or may be non-circular (termed herein as "curvilinear"). It will be apparent that in many applications, the modular energy absorbing assembly 10 may perform satisfactorily in an inverted position.

At least some of the recesses are oriented such that their floors are substantially orthogonal to a major incident component 24 (Figure 3) of the impacting force. In a given recess, the wall is inclined at an angle (α) to the major incident component of the impacting force. The angle (α) is selected so that it lies between zero and 45 degrees in order to maximize energy absorption by the wall over a given distance. The wall at least partially collapses during energy absorption, and at least some of the recesses become at least partially compressed or shatter, in some cases. In a coordinated manner arising from mutual support afforded by adjacent recesses, the assembly serves to decelerate an object that impacts with an incident force thereupon. As the wall collapses, some of the deformation occurs elastically, thereby providing at least a partial "spring-back" following initial deformation.

Thus, the invention embraces a sheet of material with recesses formed in it. The sheet remains continuous after recesses are made. Preferably, the recesses

are integral with or are monolithic with the base and sheet from which they are formed. When thermoforming is the manufacturing method of choice, it will be appreciated that wall thickness may be smaller adjacent the base than adjacent the floor of a given recess.

5 Continuing with particular reference to Figure 3, the recesses 18 of the gamma structure have imaginary central lines (C) which are spaced apart by a distance (S). The average depth of the recesses depicted in the embodiment of Figure 3 is represented by the letter (D). The reference letter (d) represents the average depth of a channel 26 which communicates with adjacent recesses. The
10 recesses are further characterized by the reference letter (W) which represents the diameter of the recess measured at the base, or basal plane 12. As illustrated, the base has a thickness represented by the reference letter (T). Another design variable is the radius (r) (Figure 3) which characterizes the joiner of a wall 20 with a channel 26.

15 It will be noted from the views of Figures 1 and 3 that the walls 20 are connected by the floor 18 of a given recess, while walls of adjacent recess are connected by the base 12 or channel 26.

Continuing with reference to Figure 3, the line 24 represents a major incident component of the impacting force, with respect to which the walls 20 are
20 inclined at an angle (α), where (α) lies between 1 and 45° . In operation, the wall at least partially collapses (or loses structural integrity by shattering). Some or all of the recesses become compressed partially elastically during energy absorption while decelerating an object that impacts thereupon.

In the preferred embodiment, at least one wall is generally shaped as
25 a frusto-conical surface and the intermediate segment has an average radius (R) of about 0.5 mm.

Impact tests have shown good results where the ratio of (D) to (W) is between about 0.5 and 0.3, while the ratio of (W) to (S) is between about 0.2 and

0.7. Good results have also been obtained when the recesses are further characterized by depth (D) to side thickness (T) ratio between about 4 and 20. Depending on the energy absorption requirements of the specific application, the depth of the channel (d) may be up to the depth (D) of the recess.

5 In various applications, experimentation has revealed that for a given geometry of recess, the inter-recess spacing (S) may affect the particular deformation characteristics. Preferably, the imaginary center (C) of at least some of the recesses is located at an apex of an equilateral triangle when viewed in the direction of the impacting object.

10 Turning now to Figures 4-5, there is depicted an alternate embodiment of the gamma structure of the invention wherein structural reinforcing ribs, rather than channels, connect at least some of the recesses.

In the preferred embodiment, the recesses may be joined by channels
26 of various depths (d) (Figure 3) and shapes. Generally, the channels 26 are
15 formed such that their depth (d) is less than the depth (D) of the floor 18 below the base 12.

Turning now to Figures 6-7, there is depicted a second alternate embodiment of the gamma structure of the present invention. In this embodiment, the modular energy absorbing assembly comprises two or more modules 30,32 which
20 are inclined with respect to each other by an angle (β). In the module 32, the recesses 20' characterized by an imaginary line C'-C' which extends orthogonally to the base 12 such that the axes C'-C' and C-C (associated with the modules 30, 32) are parallel. Upon inspection of Figures 6-7, it will be appreciated that the angle (β) essentially defines the inclination of intersection planes. In practice, however, the
25 bases of intersecting modules 30, 32 may not intersect discretely along a bend or joiner line, but instead be joined by a curvilinear intersecting segment (not shown). It may also be appreciated that the module 32 may be formed by folding a portion of the base 12 of module 30, such that the axes C'-C' may be inclined to the axes C-C.

The recesses may be shaped as truncated cones, sections of ellipsoids, sections of hyperboloids, or similar constructions, and may be of mixed shapes within a given energy absorbing module. Alternatively, at least some of the recesses are shaped as a cup, a cone, and frusto-conical body, a polyhedron, a tetrahedron, a prism, and a parallelepiped.

Continuing with reference to Figure 7, in the first module (left hand side), an angle (α) denotes the angle of inclination of the wall 20 with respect to the center line C of a representative recess. In the second module, the angle (γ) represents the inclination of wall 20' with respect to a major incident component of the impacting force 24'.

In light of this disclosure, it will be apparent that the energy absorbing characteristics of the disclosed modular energy absorbing assembly can be tailored to suit the needs of the particular application by suitable combination of depth (D) of the recess, depth (d) of the channels, inter-recess spacing (S), wall inclination (α, γ), inter-module inclination (β), and recess shape.

Turning now to Figures 8-9, there is depicted another alternate embodiment of the gamma structure of the present invention wherein the modular energy absorbing assembly 10 includes recesses that are placed at intervals which include irregular center-to-center distances across the base 12. In Figure 9, the depths of the recesses are depicted by the reference letters D', D'', D''', etc. The inter-recess space is represented by the reference letters S', S'', S''', etc. Customized angles of inclination are illustrated by the symbols α' and α'' .

Still further alternative embodiments comprehend the formation of one or more troughs or catches (not shown) that are generally defined within the bases 12 so that wires, tubes, and the like can be accommodated therein and so that one or more fluid conduits can be provided by the assembly.

Reference was made earlier to quantitative acceptance criteria which mandate that the HIC(d) value computed according to the FMVSS 201 formula shall

not exceed 1000. The table below compares HIC(d) values of the disclosed invention with the values exhibited by competitive products:

Drop Tower HIC(d) Performance
Baseline Stiffness = 1500 HIC(d); Sample Height = 20mm

Energy Absorber	HIC(d)
Invention	927
Polyurethane Foam (Prior Art) (5.5 lb ft ⁻³)	1024

10

Reference was also made above to the formation of one or more bending lines between adjacent energy absorbing modules in order to conform to abrupt contour changes of a substrate or structure to which the energy absorbing assembly is attached. The purpose of such axes is to orient an imaginary central line of the energy absorbing module substantially normally to a reaction surface. Depending upon the impact environment, these axes may either extend along the base (basal plane) or along an imaginary line connecting recesses and/or ribs.

One preferred technique for manufacturing the disclosed embodiments of the present invention is to use a thermoforming process, which begins with a thermoplastic sheet. Many types of thermoplastic resins may be used in a variety of sizes and thicknesses. Suitable materials for use in the disclosed thermoplastic process include: acrylonitrile-butadiene-styrene (ABS) resin, acetate, polycarbonate, polystyrene, polyethylene (low or high density), polypropylene, polyester, and polyvinyl chloride (PVC). Other suitable materials include any thermoplastic with an acceptable freezing range and softening character.

Sheet thickness (T) affects not only the thermoforming process steps and the characteristics of the modular energy absorbing assembly made thereby, but also significantly affects manufacturing economics. In general, less material is required to produce an assembly of the type disclosed herein when using lighter weight, thinner-gauge plastics. Conversely, the use of heavier-gauge materials requires more material, which tends to increase costs. Other things being equal, by a suitable selection of the design factors discussed herein, manufacturing economics can be realized while producing an energy absorbing assembly which is tailored to suit the needs of the particular operational environment.

Thermoforming allows the formation of gamma structures with relatively thin wall thicknesses. To achieve a thin wall section by other means, such as injection molding may, require the use of polymers having relatively high melt flows, hot molds, prolonged freezing times, and other accommodations, which tend to increase manufacturing costs.

A useful summary of conventional thermoforming arts is found in J. Florian, PRACTICAL THERMO FORMING, 2d Ed. (1996), Chs. 2-5 of which being incorporated herein by reference.

In a preferred embodiment, the composite modular energy absorbing assembly comprises one or more gamma structures 100 (Figure 10). At least one of the gamma structures has a base 12'. A plurality of recesses 16' are defined within the base 12'. At least some of the recesses 16' have one or more walls 20' that extend from the associated base 12'. Some or all of the recesses 16' have a floor 18' that may or may not define an aperture (not shown) therewithin.

Positioned in operative engagement with at least some of the gamma structures 100 are one or more delta structures 200 that are best shown in Figures 11-12. In one embodiment, at least some of the delta structures 200 have a lattice 210 of interconnected strands. The strands intersect to define a plurality of cells 220. At least some of the cells are oriented such that the plane of each cell is substantially parallel to the impacting force F (Figure 10) in order to maximize energy absorption

over a given distance. The lattice collapses partially plastically and recovers partially elastically. At least some of the cells 220 become partially closed during energy absorption.

5 It will be appreciated that a number of combinations of gamma and delta structures that are interposed with each other may be effective in realizing the energy absorption characteristics of the disclosed composite modular energy absorbing assembly. For example, stacking arrangements could include: one or more gamma structures interposed with one or more delta structures, gamma structures alone; or delta structures alone.

10 Accordingly, the disclosed composite modular energy absorbing assembly affords a more efficient energy absorber than may be realized by utilizing single structures.

15 In some embodiments, the delta structure resembles that depicted as the first structure in commonly owned U.S. Patent Number 6,199,942. In alternate embodiments, which are intended to be within the scope of the disclosed invention, the lattice of stranded cells may be configured as a crenelation, as a spiral, as a zig-zag (as depicted in commonly owned U.S. Patent Number 6,199,942 (Figure 1)), or in other forms which are adapted to achieve the objective of efficient energy absorption.

20 In one embodiment, the composite modular energy absorbing assembly includes an acoustic dampener 300 that is interposed between the gamma and delta structures.

25 In an alternate embodiment, a protrusion 310 (Figure 10) extends from one or more bases of the gamma structure 100. Each protrusion 310 is interposed between at least some of the gamma and delta structures, and serves to reduce noise and provide a cushioning arrangement therebetween. Alternatively, one or more protrusions 310 are interposed between the gamma structure 100 and a support

structure or substrate (not shown) with which the composite modular energy absorbing assembly is in operative engagement.

Continuing with reference to Figures 13-15, it will be appreciated that one or more gamma structures 100 may be stacked such that the bases 12' of adjacent gamma structures are in juxtaposition with each other. Figure 13 is a partial cross-sectional view wherein adjacent bases 12' of two gamma structures are placed in operative engagement with each other, and the associated floors 18' are spaced apart.

Figure 14 is a cross-sectional view of nested gamma structures wherein the floors 18' of adjacent gamma structures are in juxtaposition and associated bases 12' are in juxtaposition.

Optionally, the modular energy absorbing assembly, as depicted in Figure 15, may be composed of one or more gamma structures that are stacked such that the top side of a floor 18' of a gamma structure is in juxtaposition with a top side of a floor 18' of an adjacent, inverted gamma structure.

In still another embodiment of the invention, at least some of the recesses are at least partially filled with a homogenous or heterogenous medium other than air. Some of the recesses, for example, are at least partially filled with pellets. Preferably, such pellets or beads may be formed from resin, or glass, or other ceramics. Other examples of a medium which at least partially fills some of the recesses include, without limitation, ribs or channels, foams, and other fluids. Such structures have been found to change the dynamics of collapse in a favorable manner, while reinforcing the structure of the composite modular energy absorbing assembly.

In another embodiment, the fluid comprises air that is contained within a bladder which is accommodated within a recess. Alternatively, the recess itself may serve to contain the fluid.

As referenced earlier, Figures 13-15 depict alternative configurations of stacked cones. In one series of experiments, observations were made of the performance of different configurations of absorbers that have a total height of about 40 millimeters. The primary objective was to determine the relative impact performance of various stacking arrangements of two stacked 20 millimeter specimens. One stacking arrangement is depicted in Figure 13. The stacked samples were arranged in an in-line position, with the cones in line in the plan view, or offset. The performance of a 40 millimeter sandwich sample (similar to that depicted in Figure 14), and a 40 millimeter high cone sample (similar to those depicted in Figure 4) were compared. As depicted in Figure 15, the performance of two gamma structures was observed, with the two gamma structures being stacked such that the top side of a floor of a gamma structure was in juxtaposition with a topside of a floor of an adjacent, inverted gamma structure.

To assess the performance of the alternate configurations, head injury criteria (HIC(d)) were determined using a drop tower test with a constrained headform impacting at 15 mph. The results suggested that the best performers included two stacked 20 millimeter high samples with the cones facing away from each other (Figure 13). It was found that the sandwiched samples (Figure 14) performed well, but were suboptimal.

These, among other experiments, suggested that in order to optimize HIC(d), the structures can be stacked with the cones pointing away from each other and have approximately the same thickness.

While embodiments of the invention have been illustrated and described, it is not intended that these embodiments illustrate and describe all possible forms of the invention. Rather, the words used in the specification are words of description rather than limitation, and it is understood that various changes may be made without departing from the spirit and scope of the invention.

WHAT IS CLAIMED IS:

1 1. A composite modular energy absorbing assembly comprising:
2 one or more gamma structures, at least one of the gamma structures
3 having:
4 a base; and
5 a plurality of recesses defined within the base, at least some of the
6 plurality of recesses having
7 at least one wall extending from the associated base,
8 wherein at least some of the plurality of recesses are oriented such that
9 their walls are inclined at an angle α to the major incident component of the
10 impacting force, where α lies between 0 and 45 degrees, and
11 one or more delta structures positioned in operative engagement with
12 at least some of the one or more gamma structures, at least one of the delta structures
13 having:
14 a lattice of interconnected strands, the strands intersecting to define
15 a plurality of cells, at least some of the cells being oriented such that the plane of at
16 least some cells is inclined at an angle to the major component of the impacting
17 force, where the angle lies between 0 and 45 degrees in order to maximize energy
18 absorption over a given distance, at least some of the cells becoming at least partially
19 closed during energy absorption;
20 the composite assembly serving to decelerate an object that impacts
21 thereupon in order to maximize energy absorption over a given distance.

1 2. The composite modular energy absorbing assembly of claim
2 1, further including:
3 an acoustic dampener interposed between at least a portion of some
4 of the gamma and delta structures.

1 3. The composite modular energy absorbing assembly of claim
2 1, further including:
3 an acoustic dampener positioned adjacent to at least a portion of some
4 of the gamma and delta structures.

5 4. The composite modular energy absorbing assembly of claim
1, further including:

 a protrusion extending from one or more of the bases, the protrusion
being interposed between at least some of the gamma and delta structures, the
protrusion serving to reduce noise and to provide a cushioning arrangement between
10 the structures.

1 5. The composite modular energy absorbing assembly of claim
2 1, further including:

3 a protrusion extending from one or more of the bases, the protrusion
4 serving to reduce noise and to provide a cushioning arrangement between the
5 structures and a structure adjacent to the composite modular energy absorbing
6 assembly.

1 6. The composite modular energy absorbing assembly of claim
2 1, further including:

3 a protrusion extending from one or recesses, the protrusion being
4 interposed between at least some of the gamma and delta structures, the protrusion
5 serving to reduce noise and to provide a cushioning arrangement between the
structures.

1 7. The composite modular energy absorbing assembly of claim
2 1, further including:

3 a protrusion extending from one or more recesses, the protrusion
4 serving to reduce noise and to provide a cushioning arrangement between the
5 composite modular energy absorbing assembly and a structure adjacent thereto.

1 8. The composite modular energy absorbing assembly of claim
2 1, wherein the base defines one or more bend lines.

1 9. The composite modular energy absorbing assembly of claim
2 1, further including an attachment mechanism to facilitate securement of the
3 assembly to one or more other structures.

4 10. The composite modular energy absorbing assembly of claim
5 1, further including a support surface to which one or more of the bases is attached,
6 the support surface being selected from a group consisting of a pillar, a head rail, an
7 instrument panel, a seat, a seat back, a seat anti-submarine ramp, an integrated seat
8 restraint mechanism, a door panel, door-mounted hardware or beams, a dome light,
9 a console, pillar-mounted safety devices, a headliner, a bumper beam, a bumper
10 mount, a knee bolster, and a steering column.

1 11. The composite modular energy absorbing assembly of claim
2 1, further including a support surface to which one or more of the bases is attached,
3 the support surface being selected from a group consisting of a helmet, a child seat,
4 a child carriage, guards, and shock absorbers.

1 12. A composite modular energy absorbing assembly comprising:
2 one or more gamma structures, at least one of the gamma structures
3 having:
4 a base; and
5 a plurality of recesses defined within the base, at least some of the
6 plurality of recesses having
7 a floor; and
8 at least one wall extending between the base and the floor,
9 wherein at least some of the plurality of recesses are oriented such that
10 their walls are inclined at an angle α to the major incident component of the
11 impacting force, where α lies between 0 and 45 degrees.

1 13. The composite modular energy absorbing assembly of claim
2 12, wherein at least some of the floors define an aperture therein.

1 14. The composite energy absorbing assembly of claim 12,
2 wherein at least some of the recesses are shaped as a cup, a cone, a frusto-conical
3 body, a polyhedron, a tetrahedron, a prism, a parallelepiped, a truncated cone, a
4 section of an ellipsoid, a section of an hyperboloid, and mixtures of such shapes.

1 15. The composite modular energy absorbing assembly of claim
2 12, wherein the one or more gamma structures are stacked such that the bases of
3 adjacent gamma structures are in juxtaposition with each other.

1 16. The composite modular energy absorbing assembly of claim
2 12, wherein the one or more gamma structures are stacked such that the floors of
3 adjacent gamma structures are in juxtaposition with each other.

1 17. The composite modular energy absorbing assembly of claim
2 12, wherein the one or more gamma structures are stacked such that the topside of
3 a floor of a gamma structure is in juxtaposition with a topside of a floor of an
4 adjacent, inverted gamma structure.

1 18. A composite modular energy absorbing assembly comprising:
2 one or more gamma structures, at least one of the gamma structures
3 having:
4 a base; and
5 a plurality of recesses defined within the base, at least some of the
6 plurality of recesses having
7 at least one wall extending from the base,
8 wherein at least some of the plurality of recesses are oriented such that
9 their walls are inclined at an angle alpha to the major incident component of the
10 impacting force, where alpha lies between 0 and 45 degrees.

1 19. The composite modular energy absorbing assembly of claim
2 18, wherein at least some of the recesses are at least partially filled with a fluid.

1 20. The composite modular energy absorbing assembly of claim
2 18, wherein at least some of the recesses are at least partially filled with pellets.

21. The modular composite energy absorbing assembly of claim 19, wherein the fluid comprises a filler material disposed at least partially within the energy absorbing module, the filler material being selected from the group consisting of a pelletized material, a granular material, a foam, a gas, and mixtures thereof.

22. A composite modular energy absorbing assembly comprising:
one or more delta structures positioned in operative engagement with each other, at least one of the delta structures having:
a lattice of interconnected strands, the strands intersecting to define a plurality of cells, at least some of the cells being oriented such that the plane of at least some cells is inclined at an angle to the major component of the impacting force, where the angle lies between 0 and 45 degrees, in order to maximize energy absorption over a given distance, at least some of the cells becoming at least partially closed during energy absorption.

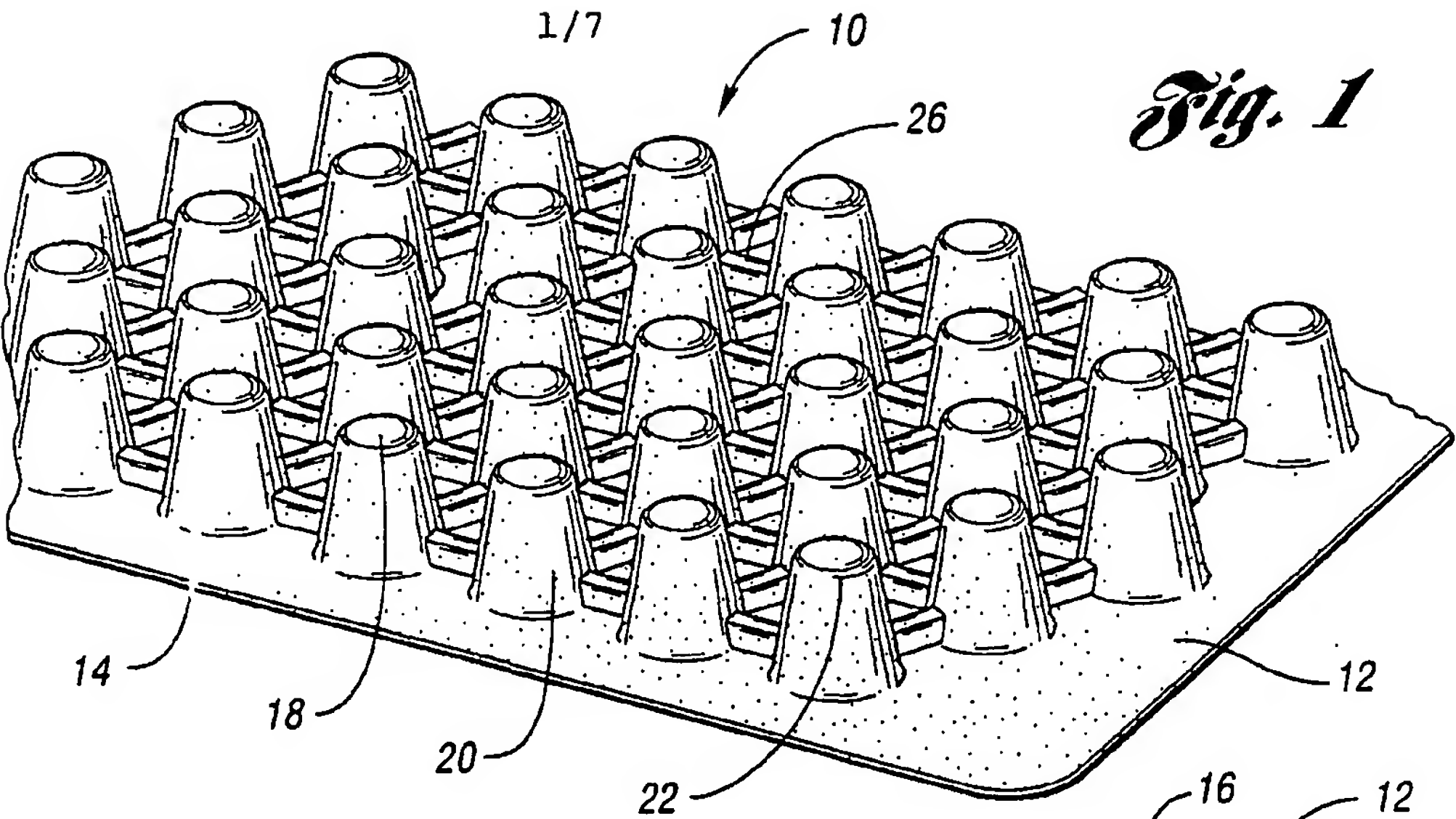
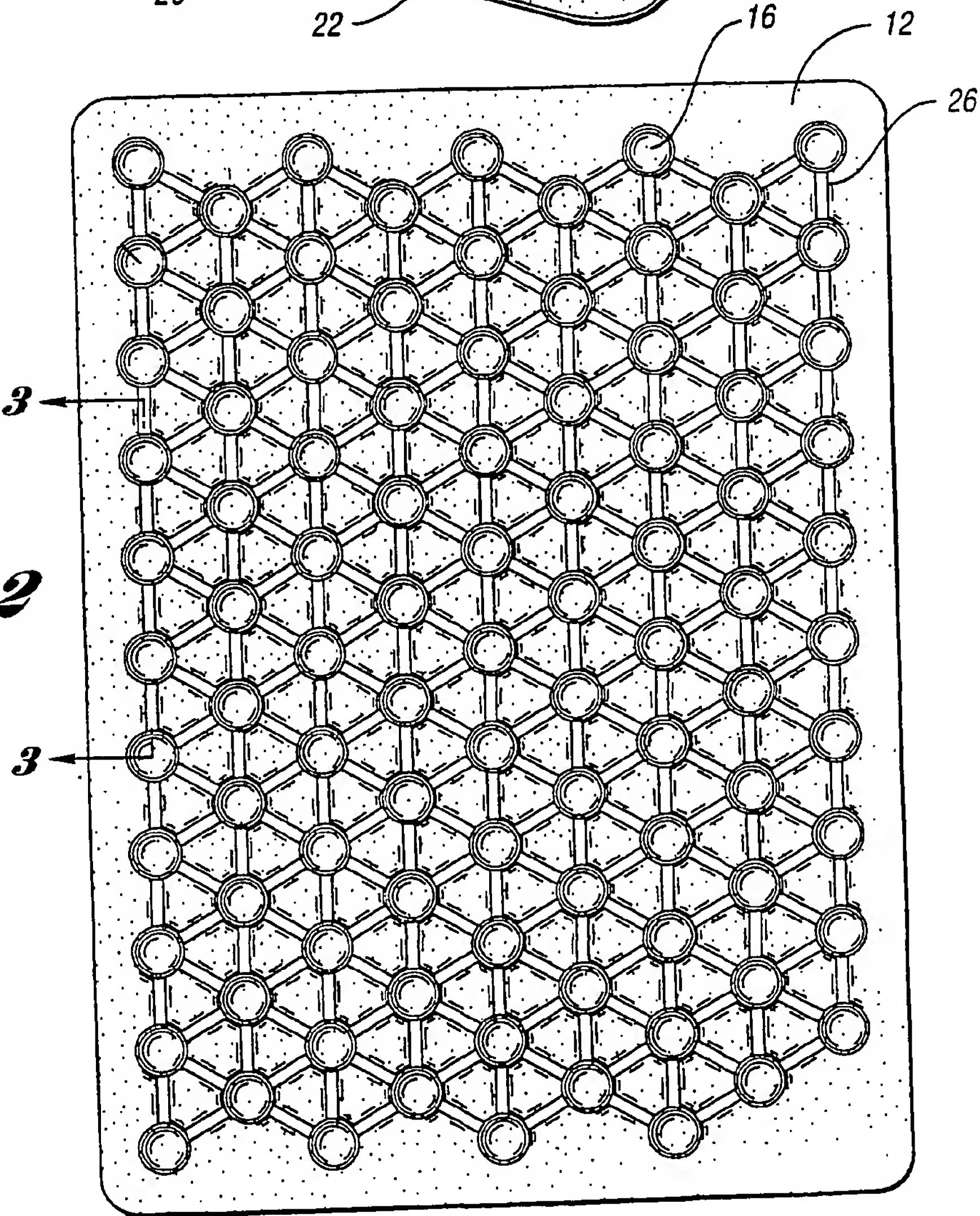


Fig. 2



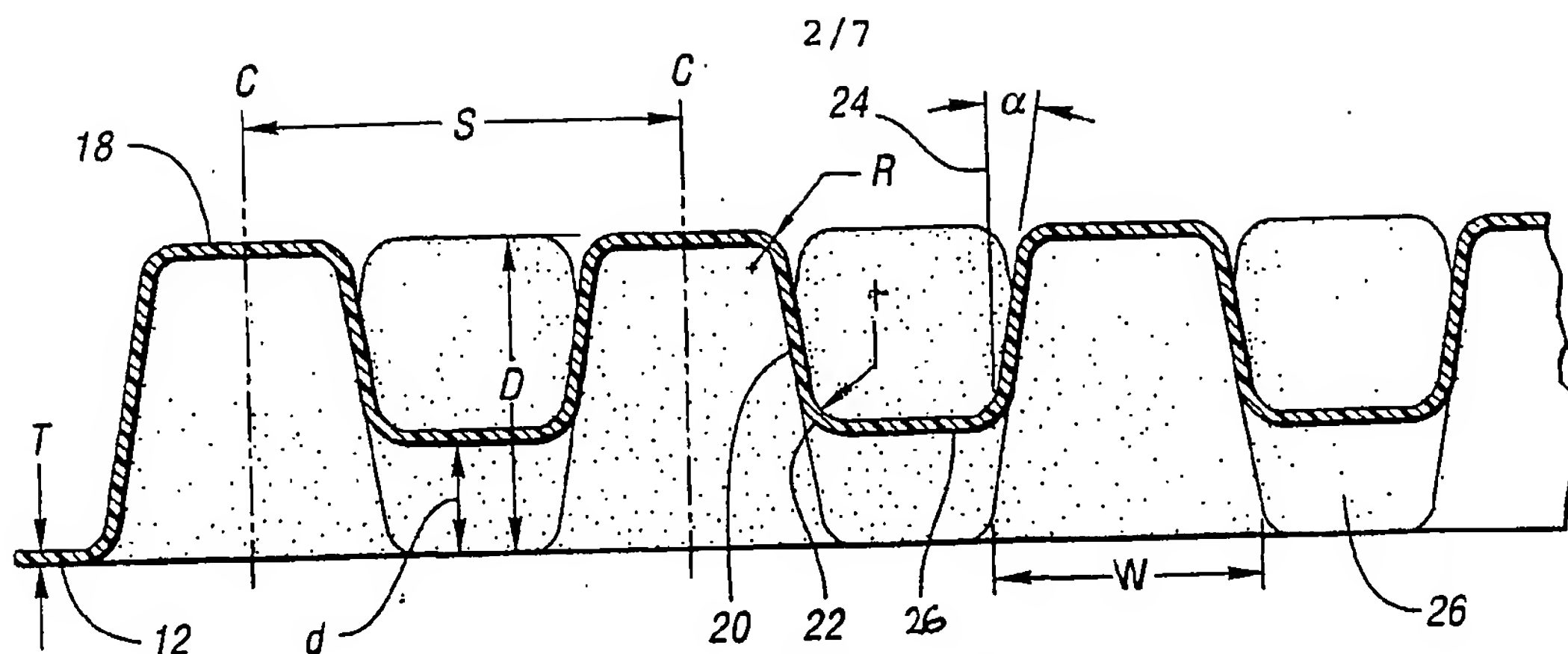


Fig. 3

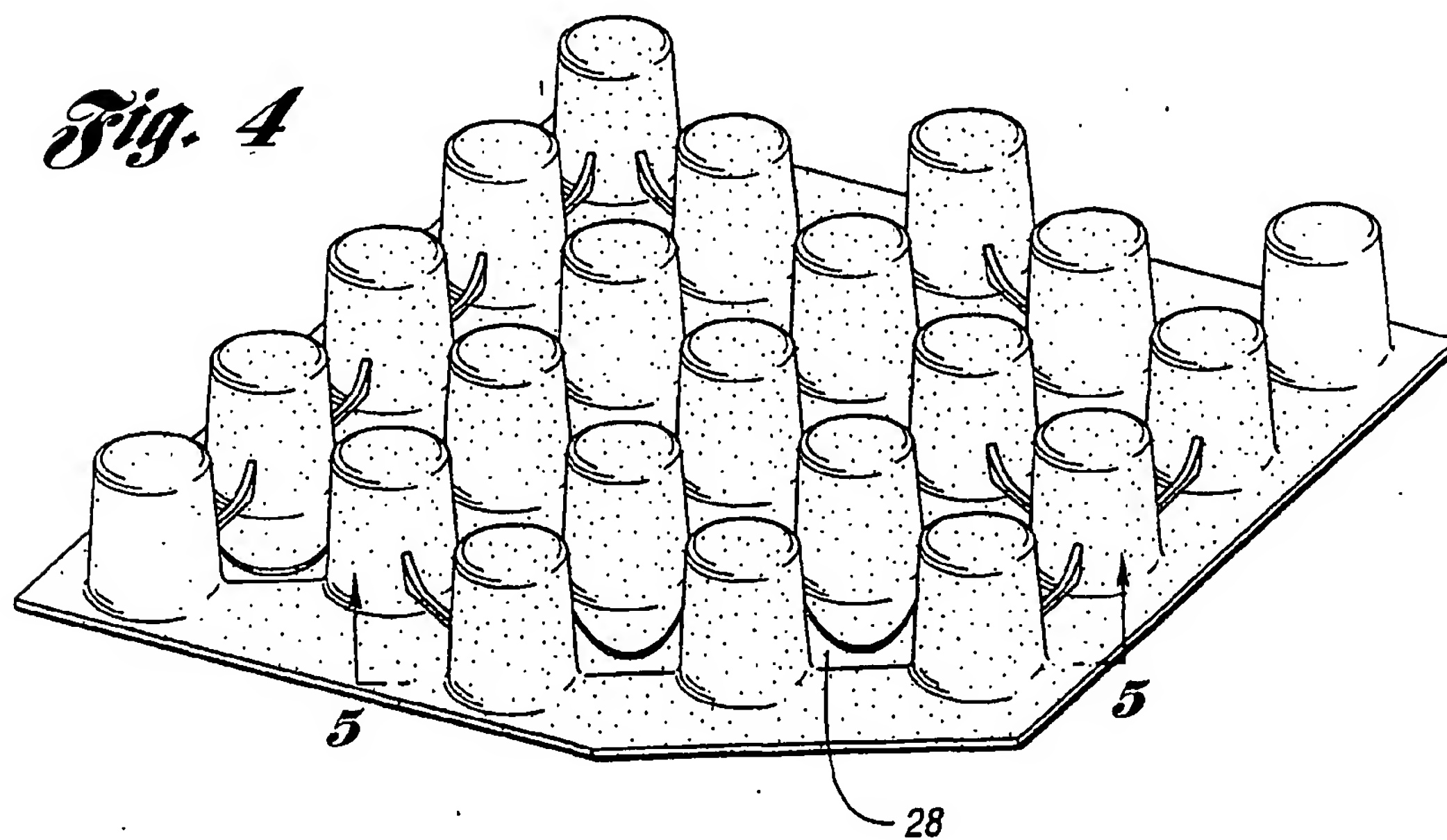


Fig. 4

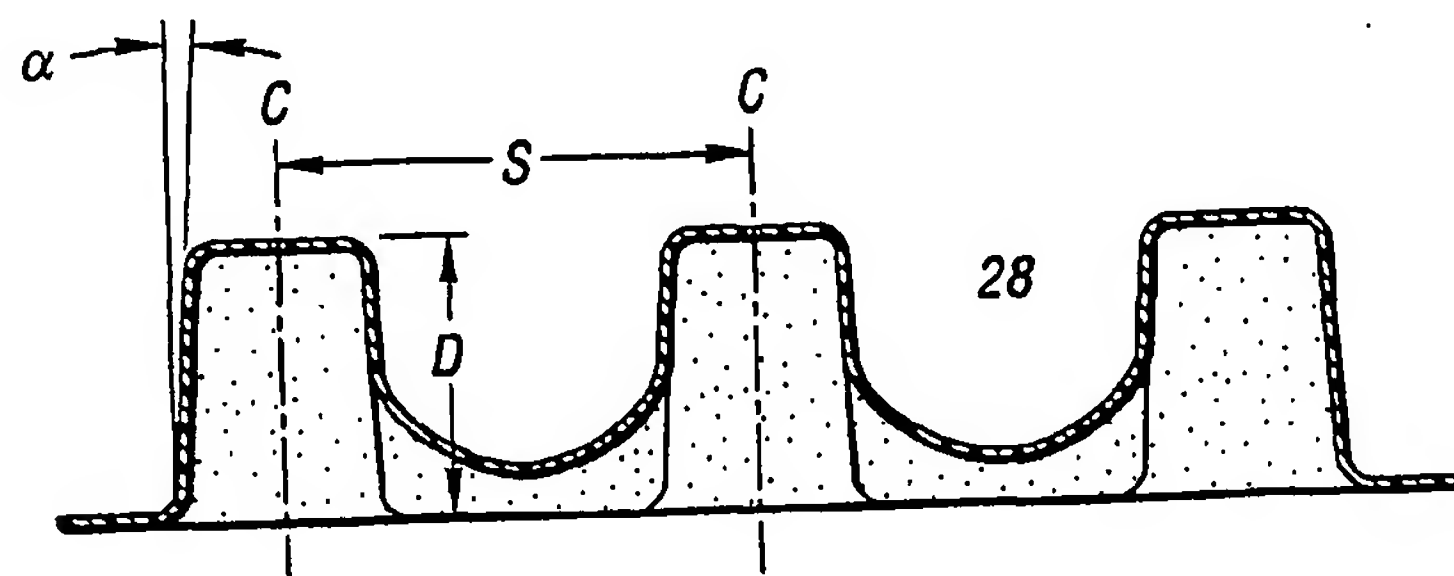


Fig. 5

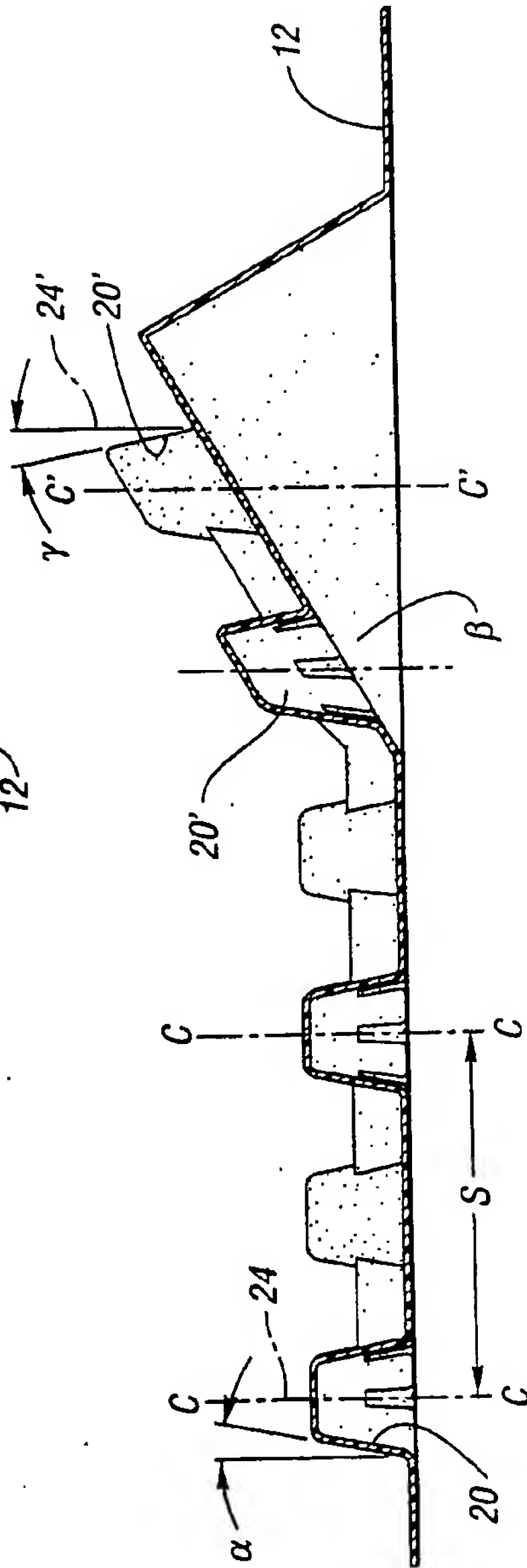
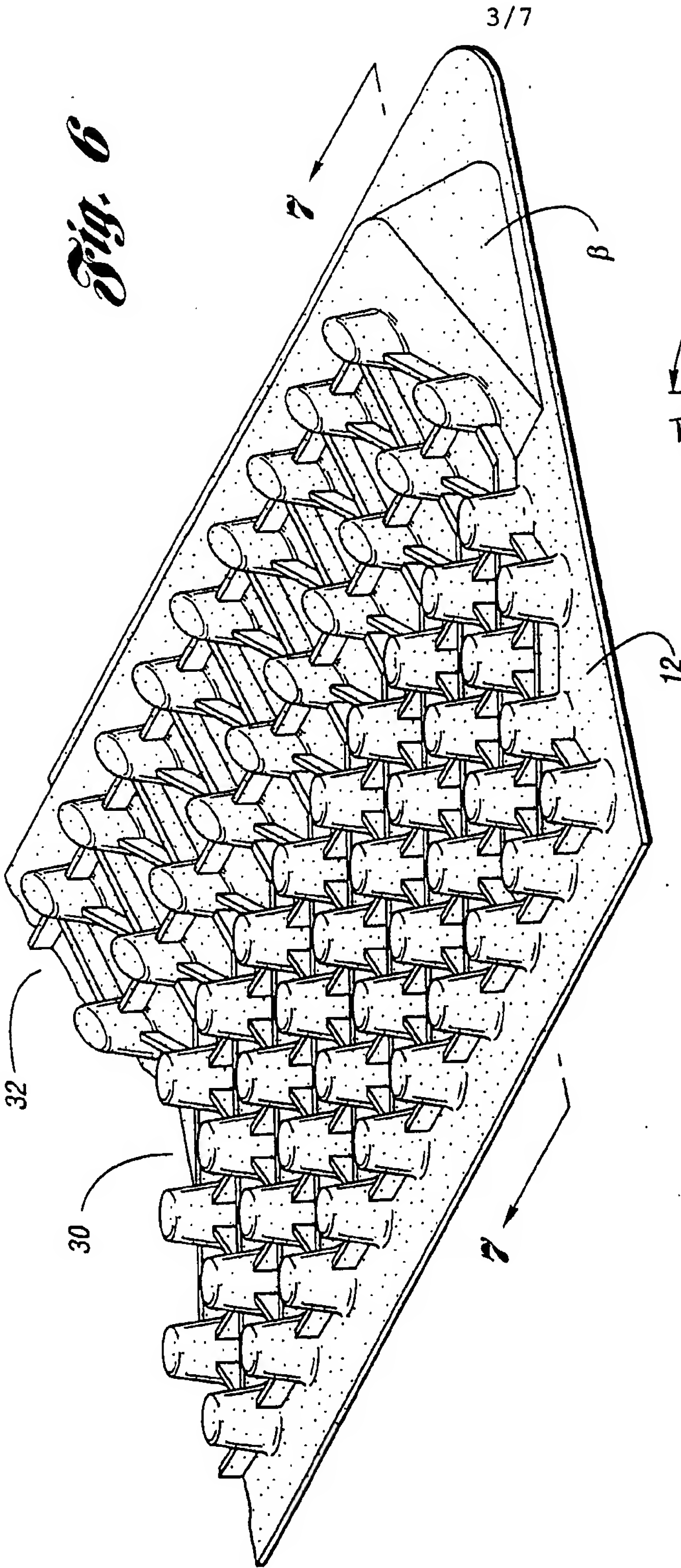


Fig. 7

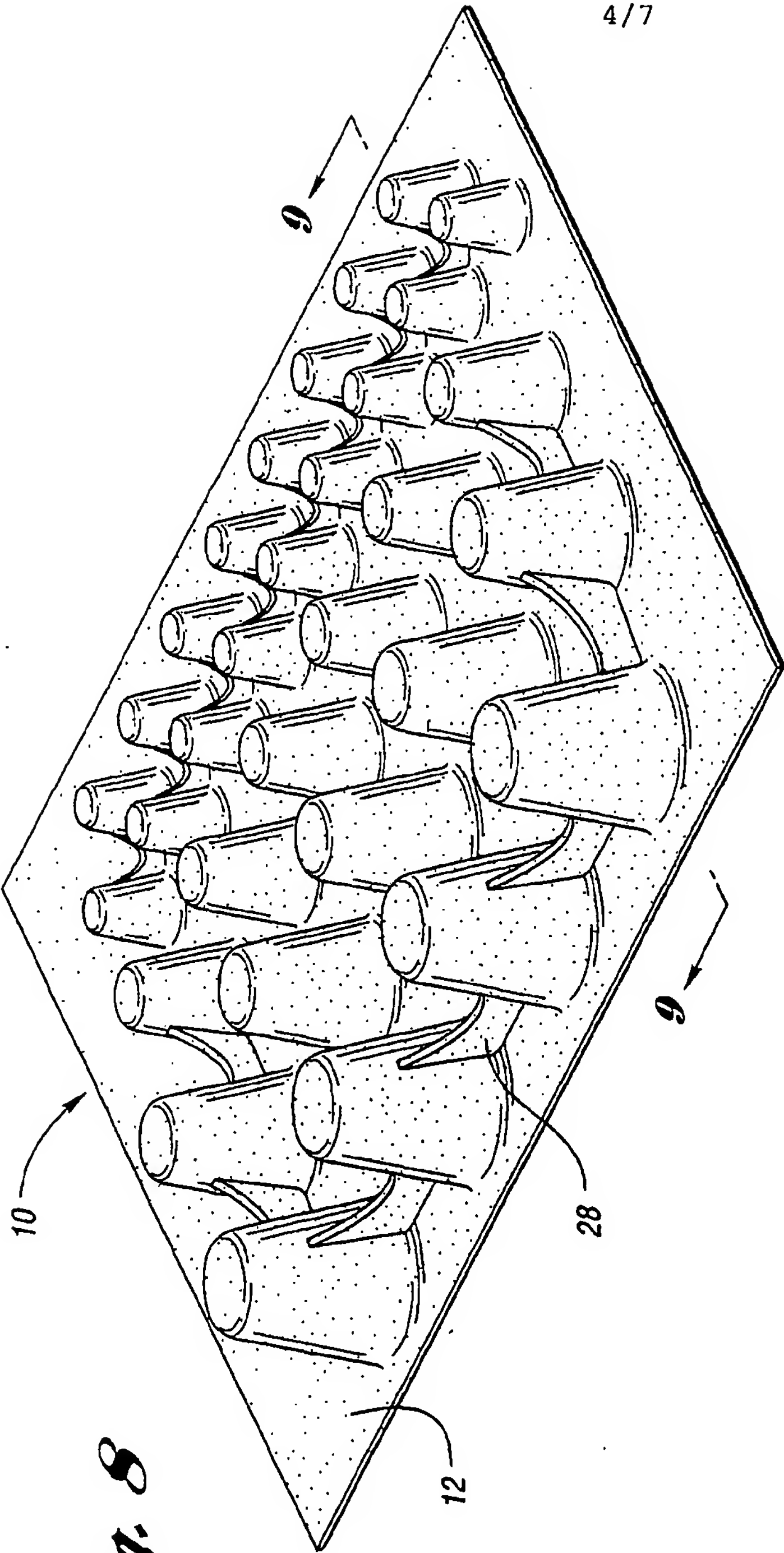


Fig. 8

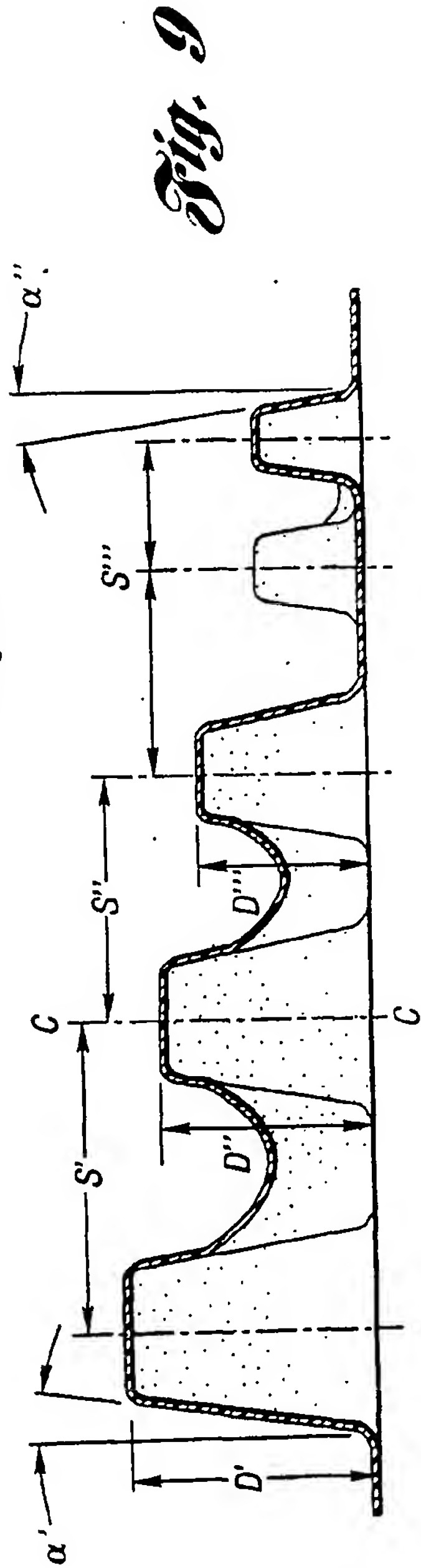


Fig. 9

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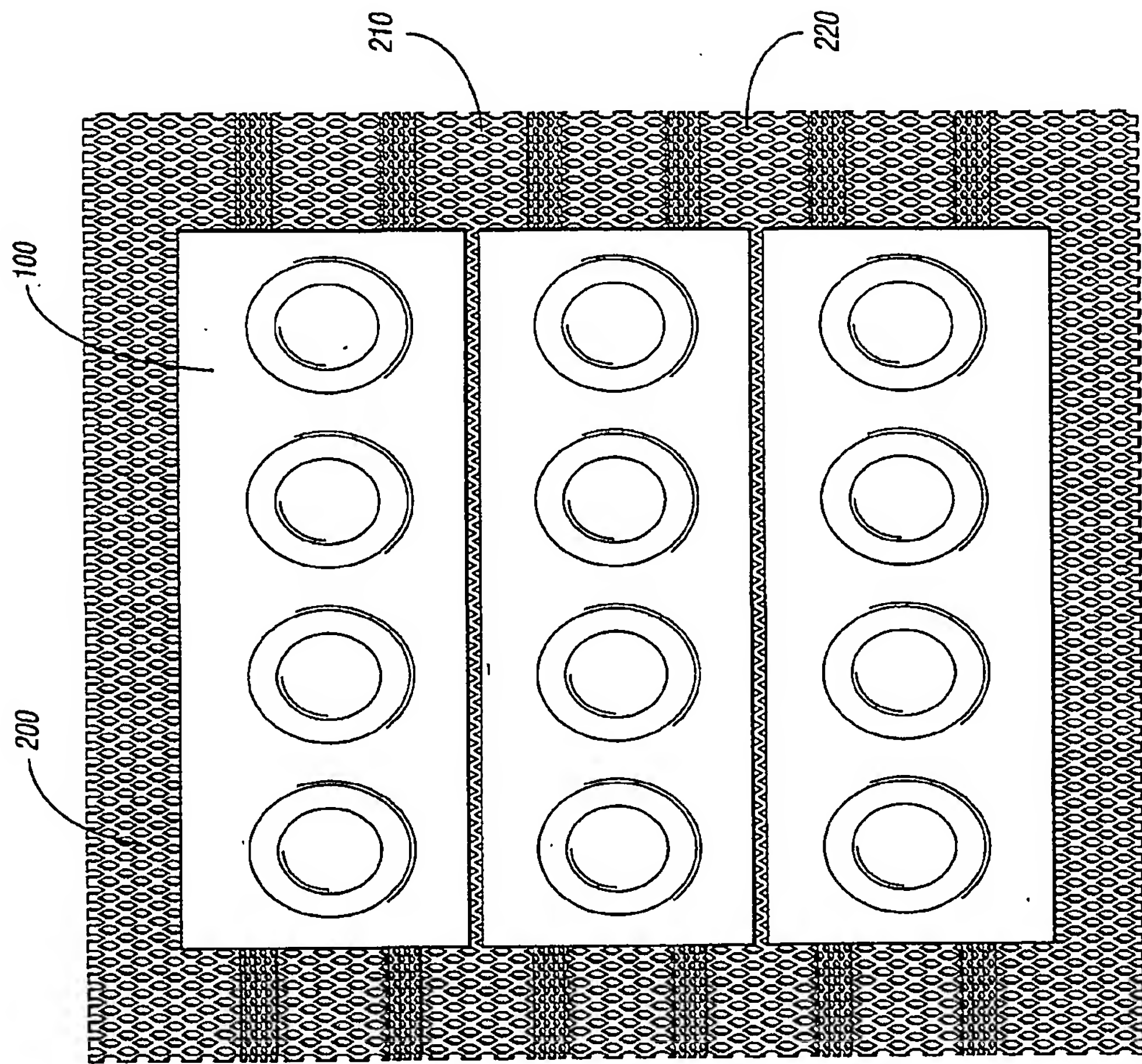


Fig. 11

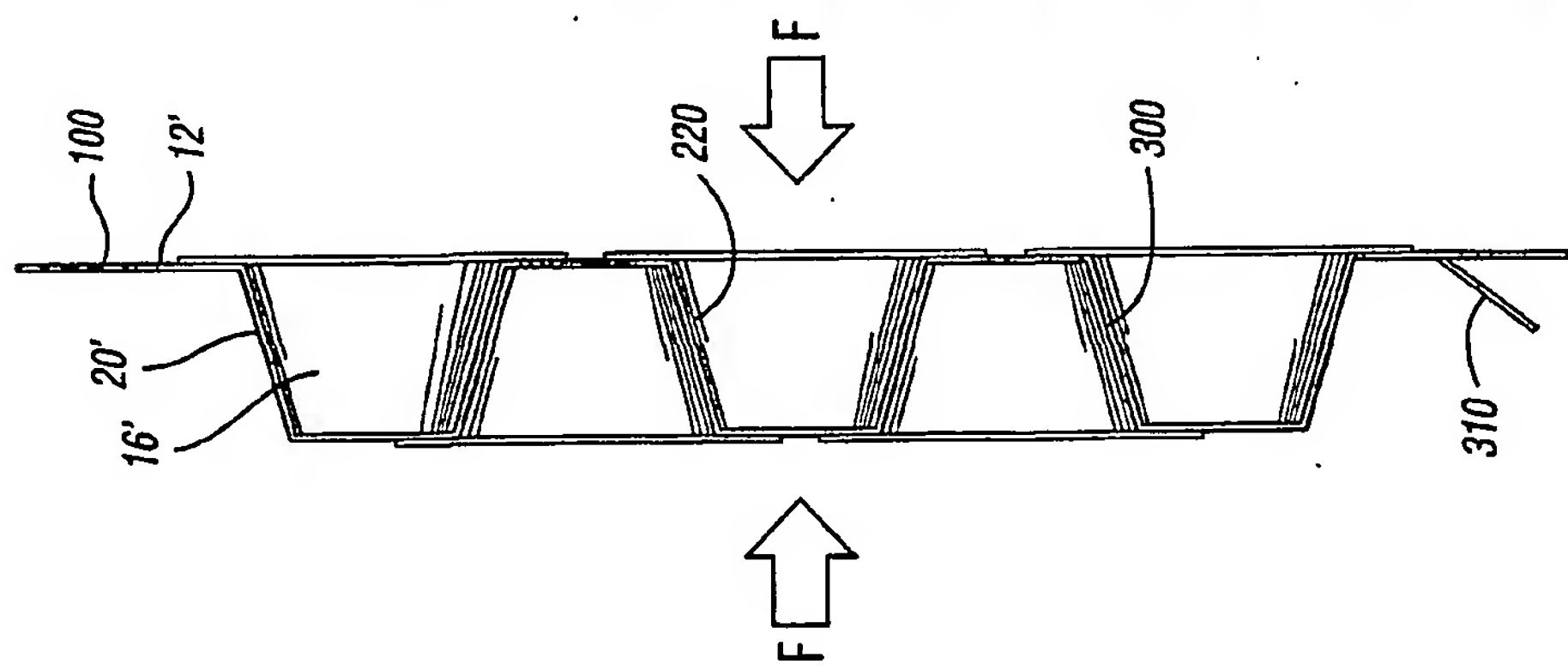


Fig. 10

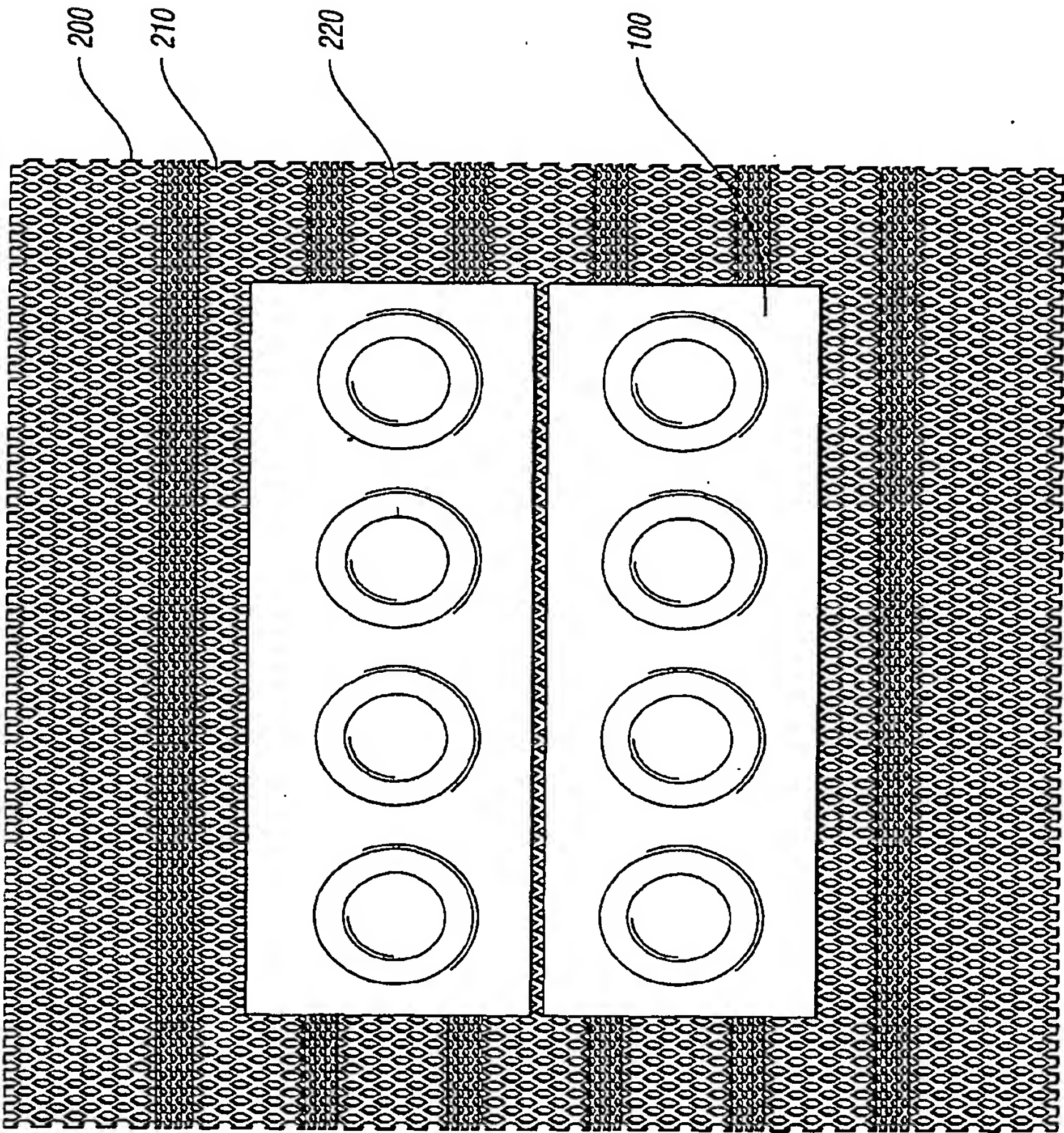


Fig. 12

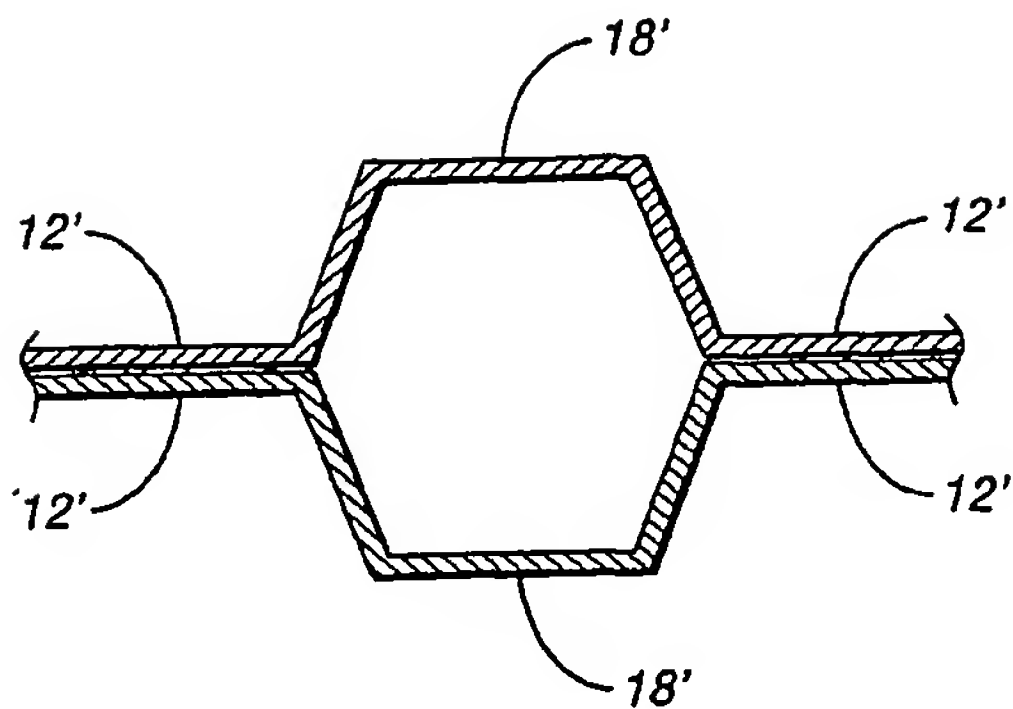


Fig. 13

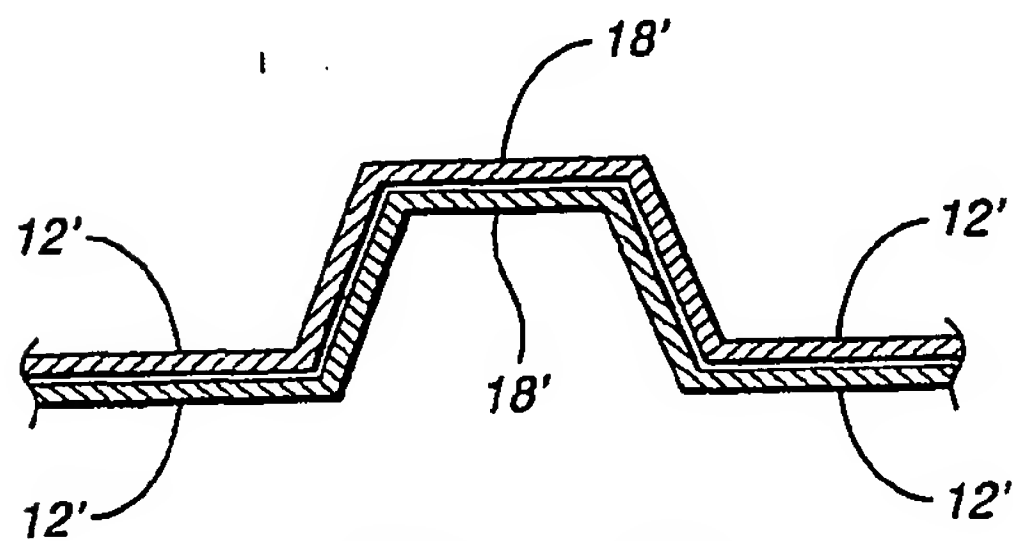


Fig. 14

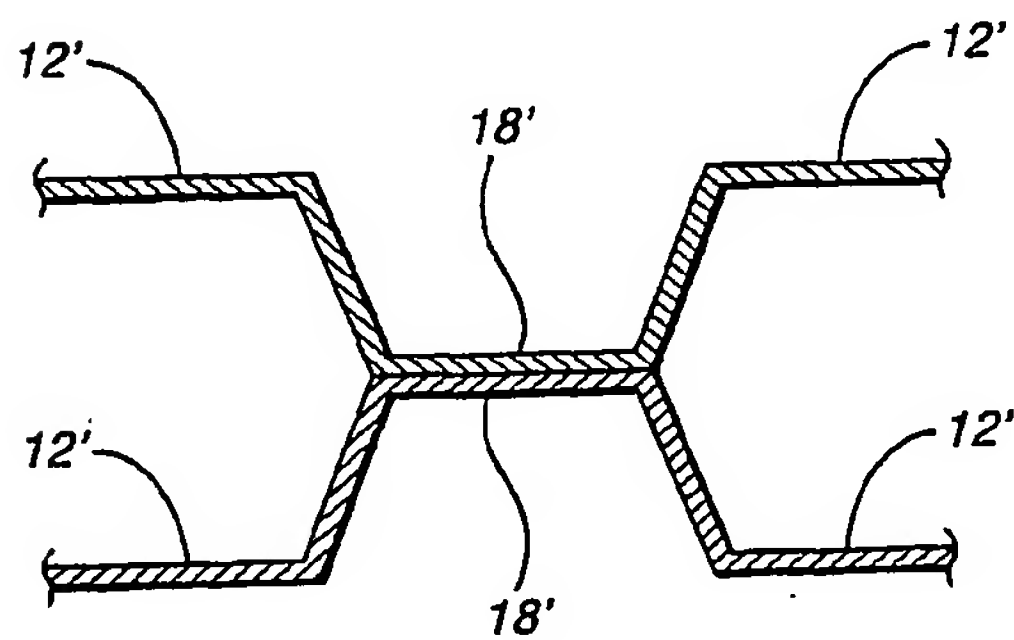


Fig. 15

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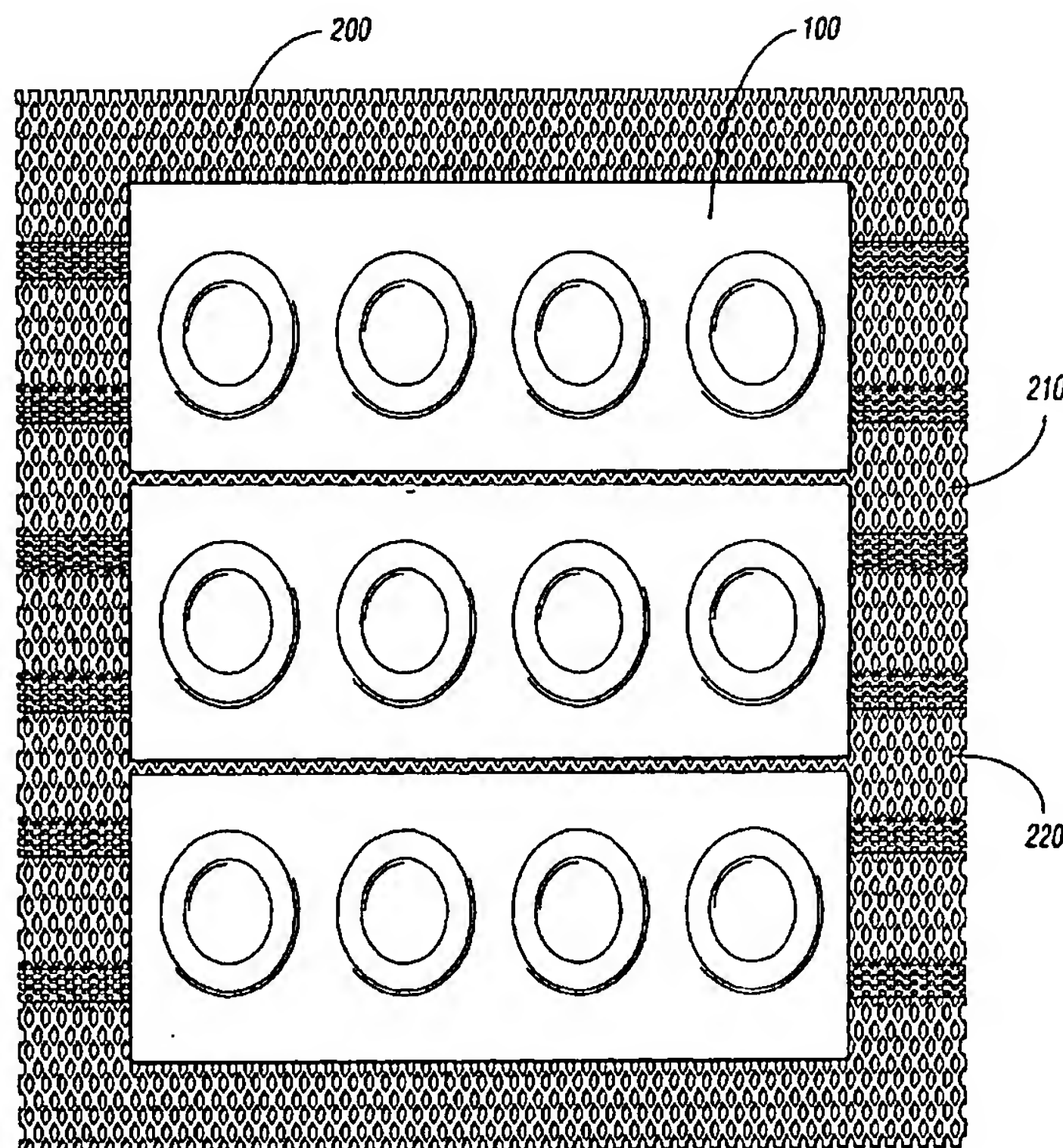
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[Continued on next page]

(54) Title: **COMPOSITE ENERGY ABSORBER**



(57) Abstract: A composite modular energy absorbing assembly with one or more gamma structures 100 that are interposed with one or more delta structures 200. The gamma structures have a base 12' and a plurality of recesses 16' defined therewithin. The recesses 16' have at least one wall 20' extending from the associated base 12'. At least some of the recesses 16' are oriented such that their walls are substantially parallel to a major incident component of an impacting force. The walls 20' collapse. The delta structures 200 have a lattice 210 of interconnected strands which intersect to define a plurality of cells 220. The plane of at least some of these cells are substantially parallel to the impacting force. The lattice collapses during energy absorption. The composite assembly serves to decelerate an object that impacts thereupon in order to maximize energy absorption over a given distance. In alternate embodiments, stacking arrangements include: gamma structures alone; or delta structures alone.

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A. CLASSIFICATION OF SUBJECT MATTER

IPC(7) : B60R 21/04; B32B 1/00

US CL : 296/189, 296/39.1; 293/133; 280/751; 188/371; 428/178, 428/175, 428/166

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

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U.S. : Please See Continuation Sheet

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 3,231,454 A (WILLIAMS) 14 April 1966 (14.04.1966), Figure 7.	12-15, 18
X	US 4,631,221 A (DISSELBECK et al.) 23 December 1986 (23.12.1986), Figure 4.	12, 16, 18
X	US 5,731,062 A (KIM et al.) 24 March 1998 (24.03.1998), see total document.	12, 17, 18
X	US 5,518,802 A (COLVIN et al.) 21 May 1996 (21.05.1996), see total document.	18, 19, 21
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Y		20
Y	US 3,782,767 A (MOORE) 01 January 1974 (01.01.1974), column 8, line 30.	20
X	US 5,500,037 A (ALHAMAD) 19 March 1996 (19.03.1996), Figure 4.	22

☐ Further documents are listed in the continuation of Box C.

☐ See patent family annex.

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Continuation of B. FIELDS SEARCHED Item 1:

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